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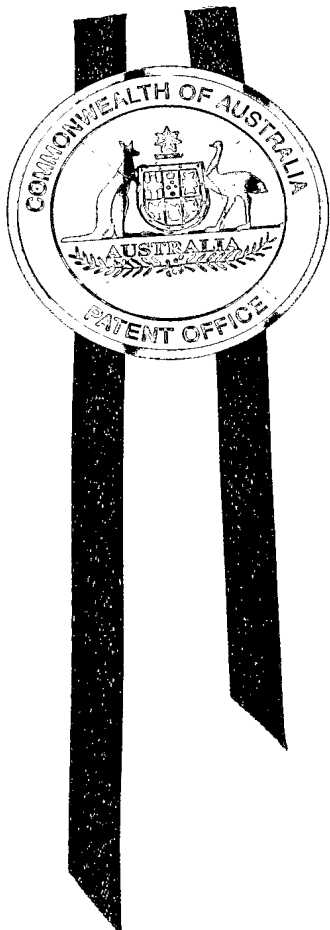


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I, LEANNE MYNOTT, MANAGER EXAMINATION SUPPORT AND SALES hereby certify that annexed is a true copy of the Provisional specification in connection with Application No. 2004901481 for a patent by COMMONWEALTH SCIENTIFIC AND INDUSTRIAL RESEARCH ORGANISATION and THE BOEING COMPANY as filed on 19 March 2004.



WITNESS my hand this
Eleventh day of March 2005

A handwritten signature in black ink, appearing to be 'L. Mynott'.

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Patents Act 1990

PROVISIONAL SPECIFICATION

Applicant(s):

COMMONWEALTH SCIENTIFIC AND INDUSTRIAL RESEARCH
ORGANISATION

THE BOEING COMPANY

Invention Title:

ACTIVATION METHOD

The invention is described in the following statement:

ACTIVATION METHOD

FIELD OF THE INVENTION

The present invention relates to a method of
5 activating an organic coating, a coated substrate having
an activated coating and an activation treatment for an
organic coating. In particular, the activation method
improves the adhesion of the organic coating to further
coating layers and/or to other entities.

10

BACKGROUND OF THE INVENTION

Organic coatings are generally used to protect the
surface of materials from incidental damage, abrasion,
chemical attack and from environmental or in-service
15 degradation. Organic coatings are also used to enhance
the aesthetics and/or optical properties of an object or
component.

The surface properties of many coatings dramatically
change on drying, curing and/or aging to become more inert
20 than might be predicted based on the chemistry of their
individual components alone. Whilst this phenomenon in
part provides the coating with chemical resistance, impact
strength and abrasion resistance, it also complicates the
process of applying additional coating layers,
25 particularly when they are not applied within a
predetermined reapplication window. The same problem
arises with applying other entities such as sealants,
fillers, stickers and the like, to such coatings. In cases
which require the application of additional coating layers
30 and/or other entities, a mechanical or stripping process
of the coating is generally necessary before the re-
application procedure can take place.

In the specific example of aircraft coatings, it is
well known that adhesion will not meet in-service
35 performance requirements when fresh layers of coating are
applied over layers which have aged beyond the acceptable
reapplication window. The acceptable window may be of the

order of days under ambient conditions or hours under conditions of high temperature and/or humidity. Once the reapplication window has been exceeded, the standard practice for applying additional coating layers on
5 aircraft involves mechanical abrasion of the aged coating.

Both chemical stripping and mechanical abrasion have limitations. Mechanical abrasion is labor intensive, the reproducibility is variable, and it is ergonomically costly due to the highly repetitive and vibratory nature
10 of the work. As such there is a pressing need for the development of a surface treatment to improve the adhesion of aged or inert industrial organic coatings towards additional coating layers or other entities, for example, adhesives, sealants, fillers, stickers and the like.

15 Haack (*Surface and Interface Anal*, (2000), 29, p829) investigated the interaction of automotive polyurethane coatings using UV light to generate ozone. Promising results in terms of improved adhesion and reduced water contact angles were produced when paint formulations
20 incorporating TiO_2 were subjected to H_2O_2 and UV light. However, there are obvious practical difficulties associated with this strategy, particularly in terms of its commercial viability for application in areas susceptible to corrosion and for treating larger surfaces.
25 Also the occupational health and safety issues make it less suited to commercial application.

Coating manufacturers have developed a method of improving the procedure of coating stripping through the development of barrier layers which, for example, protect
30 the primer and conversion coating of metal structures from the chemical stripping agents (US 6,217,945). Although this procedure would inevitably improve the rate of paint stripping and reduce the amount of infrastructure down time it still relies on paint removal to provide a surface
35 which will accept a fresh coating layer with acceptable adhesion.

In the biological field, Park et al. (*Biomaterials*, (1998), 19, p851) employed the surface urethane NH group to graft chemical species onto polyurethane rubber, whilst Levy et al. (*Biomaterials* (2001) 22, p2683) employed a strong base to remove the surface urethane NH proton to accelerate such nucleophilic grafting reactions. Both strategies are unsuitable for activating organic coatings. The chemical reaction kinetics of the first strategy would be too slow to be practical, particularly since, considering the low surface energy and inertness to bonding of such coatings, the urethane NH groups may not be oriented towards the air-coating interface. The use of very strong bases, as per the second strategy, may degrade existing paint layers, resulting in a mechanically weak foundation for fresh coatings to adhere to. Furthermore, the latter strategy is also unacceptable for activating large areas due to corrosion and health and safety considerations.

Other strategies in the biological field have employed free radical techniques to graft molecules onto the surface of biomedical polyurethane surfaces (Matuda et al, *J. Biomed. Res.*, (2002), 59, p386; Eaton et al, *Biomaterials*, (1996), 17, p1977). Although commercially viable, the main difficulty with this strategy lies in promoting actual grafting of the substrate.

Controlled glycolysis or aminolysis as described in *Polymer Engineering & Science* (1978), 18, p844, and *J. Applied Polymer Science* (1994), 51, p675) has very slow kinetics at room temperature and as such is not a practical solution. The use of reagents such as dimethyl phosphonate (*Polymer Degradation and Stability*, (2000), 67, p159) is also not appropriate since they are highly toxic and act too slowly at room temperature.

The strategies disclosed above do not adequately address the need for the development of a surface treatment to improve the adhesion of aged or inert organic coatings to additional coating layers and/or other

entities. The problems of commercial viability, health and safety considerations, viable kinetics, applicability to small and large surface areas still remain and need to be resolved.

5

SUMMARY OF THE INVENTION

We have now found a method which allows the activation of organic coatings to improve their adhesive properties towards further coating layers of the same or different type, and/or other entities without compromising coating integrity, via the use of mild reagents and conditions.

The term "mild" in this context refers to chemicals which are not known to be excessively corrosive, acidic, basic or toxic and are applicable for use in highly regulated industrial environments. One example of such an environment is a commercial aircraft paint hangar.

Advantageously, this method no longer requires the traditional methods of mechanical abrasion or chemical stripping of an organic coating to improve its adhesive properties towards additional coatings and/or other entities.

In a first aspect, the present invention provides a method of activating an organic coating to enhance adhesion of the coating to a further coating and/or to other entities comprising applying a solvent and an adhesion promoter either simultaneously, separately or sequentially to a surface of the organic coating, wherein contact of the organic coating with the solvent or the solvent and adhesion promoter combination results in swelling of the organic coating.

In another aspect, the present invention provides a coated substrate having an activated coating, wherein the adhesive properties of a surface of the activated coating have been enhanced by application of a solvent and an adhesion promoter to the coating, either simultaneously, separately or sequentially.

Advantageously, the solvent and adhesion promoter are combined and applied to the organic coating in the form of an activation treatment.

5 In a further aspect, the present invention provides an activation treatment for an organic coating comprising an adhesion promoter and a solvent, wherein application of the solvent or the solvent and adhesion promoter combination to a surface of the organic coating results in swelling of the organic coating, thus enhancing the
10 adhesion of the surface of the organic coating to a further coating and/or to other entities.

In a further aspect, the present invention provides a method for the preparation of the activation treatment defined above comprising the step of mixing the solvent
15 with an adhesion promoter.

DETAILED DESCRIPTION OF THE INVENTION

In this specification, except where the context requires otherwise due to express language or necessary
20 implication, the word "comprise" or variations such as "comprises" or "comprising" is used in an inclusive sense, i.e. to specify the presence of the stated features but not to preclude the presence or addition of further features in various embodiments of the invention.

25 As used in the specification the singular forms "a" "an" and "the" include plural references unless the context clearly dictates otherwise. Thus, for example, reference to "a solvent" includes mixtures of solvents, reference to "an adhesion promoter" includes mixtures of
30 two or more such adhesion promoters, and the like.

The method of the present invention involves activating an organic coating so as to enhance the adhesive properties of at least the surface of the coating towards additional coating layers and/or other entities,
35 for example, adhesives, sealants, fillers, stickers and the like. The term 'activating' is used in this context to mean the improvement of the adhesive properties of the

organic coating relative to the adhesive properties of that coating, prior to application of the solvent and adhesion promoter.

The word "coating" is used herein its broadest sense and describes decorative topcoats; undercoats; intermediate coatings; primers; sealers; lacquers; coatings which are pigmented or clear; coatings designed for specific purposes, such as, corrosion prevention, temperature resistance, or camouflage; coatings which are high gloss, matte, textured, or smooth in finish; or coatings containing specialty additives, such as, metal flakes.

In general, organic coatings which are cured, dried or aged beyond a certain time period develop resistance to forming strong adhesive linkages towards other entities. Their surface properties become more inert than might be predicted, based on the chemistry of their individual components alone. Without wishing to be limited by theory, it is believed that this phenomena may result from a reduction in coating surface energy and amount of reactive surface functional groups in conjunction with a higher cross-link density as a function of cure time/aging which makes chemical interaction and/or the formation of strong adhesive linkages with other entities difficult.

The organic coatings to which the present invention may be applied include, but are not limited to, fully or partially cross-linked organic coatings. Examples of organic coatings include, polyurethane, epoxy, polyester and/or acrylic coatings, more preferably polyurethane coatings. Due to their superior mechanical properties and resistance to abrasion, chemical attack, and environmental degradation, such organic coatings are widely used to protect infrastructure in the aerospace, marine, military, automotive, and construction industries. Many of these coatings show a marked reduction in adhesion to other entities, such as additional coating layers, adhesives,

sealants, stickers, and the like, with increased time of curing and/or aging.

The activation method involves applying the activation treatment or the components thereof to a surface of the organic coating. The surface treatment is not a primer coating but rather a chemical method of modifying the surface of the existing coating so that it is more receptive to forming adhesive interactions with further coatings and/or other entities.

Without wishing to be limited by theory, it is believed that a suitable choice of solvent(s) and/or solvent(s)-adhesion promoter(s) combinations allows the coating to be reversibly swollen (expanded). This allows the adhesion promoter(s) to penetrate the highly-chemically-resistant coating surface and engage in attractive interactions with the existing coating, for example molecular entanglement, physiochemical interactions such as hydrogen bonding, or chemical linkages such as covalent or ionic bonds. Upon evaporation or partial evaporation of the solvent(s) and/or adhesion promoter(s), the coating surface is left disordered, with at least some of the securely-tethered functional adhesion promoters protruding from the surface and hence available to form adhesive linkages with separate entities through molecular entanglement, physiochemical, or chemical interactions.

Preferably the activation treatment or components thereof only swell the surface of the organic coating so that the integrity of the coating is not compromised.

The solvent may be a single solvent or a combination of two or more solvents. Preferably the solvent is an organic solvent. Suitable organic solvents or solvent combinations include ester based solvents such as ethyl acetate, propyl acetate, isopropyl acetate, butyl acetate, isobutyl acetate and tertiary butyl acetate; ketones such as methyl ethyl ketone, methyl amyl ketone, methyl isoamyl ketone, methyl isobutyl ketone and acetone; tetrahydro

furan alcohols such as benzyl alcohol; tertiary butanol; isopropanol ethers such as ethylene glycol dimethyl ether, ethylene glycol monomethyl ether, diethylene glycol monomethyl ether, diethylene glycol dimethyl ether and
5 methyl ether of propylene glycol; amides such as N-methyl pyrrolidinone; aromatics such as toluene; and halogenated solvents such as dichloromethane and tetrachloroethylene. However, in view of the toxicity and negative
environmental impact of halogenated solvents, it will be
10 understood that they should be used within the constraints of environmental, health, and safety regulations.

More preferred solvents are ester based solvents such as ethyl acetate, isopropyl acetate and/or tertiary butyl acetate; ketone solvents such as methyl amyl ketone and/or
15 methyl isoamyl ketone; alcohols such as benzyl alcohol and/or ethylene glycol monomethyl ether; ether solvents such as ethylene glycol dimethyl ether and/or tetrahydrofuran; amide solvents such as N-methyl pyrrolidinone; chlorinated solvents such as
20 dichloromethane and/or dichloroethylene. More preferred solvent combinations include high and low boiling point solvent combinations such as N-methyl pyrrolidinone: ethyl acetate; dichloromethane: benzyl alcohol; ethyl acetate: benzyl alcohol; ethyl acetate: benzyl alcohol; ethyl
25 acetate: diglycol ether dimethyl ether.

Particularly preferred solvents are ester based solvents such as ethyl acetate and/or isopropyl acetate; and ketone solvents such as methyl amyl ketone and/or methyl isoamyl ketone.

30 The solvent(s) are generally present in the activation treatment in an amount of less than about 99.99%, preferably greater than about 50%, most preferably in an amount between 50 and 99% based on the total weight of the activation treatment or the combination of
35 solvent(s), adhesion promoter(s) and any optional additive(s).

The adhesion promoter is preferably a compound having at least one functional group. Preferably, two or more functional groups are present and under these circumstances they can be of the same or different
5 functionality. Examples of such functional groups include but are not limited to amines, alcohols, carboxylic acid, amide, ester, thiol, ether, epoxy, isocyanate, isothiocyanate and anhydride groups. Adhesion promoters with nucleophilic functional groups are preferred.
10 Particularly preferred are adhesion promoters with functional groups based on amines and/or alcohols.

The adhesion promoter may take the form of a linear molecule, or alternatively it may take a branched, hyperbranched or dendritic structure. It may be a
15 discrete molecule or a polymer with a molecular weight distribution.

Adhesion promoters with molecular weights less than about 100,000 have been found to be suitable. Preferably, the molecular weight is less than about 10,000 to achieve
20 suitable activation kinetics.

Suitable adhesion promoters include linear and branched polyethylene imines; amine, epoxy, isocyanate and/or hydroxyl terminated polyether glycols such as polyethylene glycol, polypropylene glycol and/or
25 polyethylene oxide; dendrimers such as polypropylene imine octamine dendrimer and/or polypropylene imine tetraamine dendrimer; and smaller molecular weight amines such as ethylene diamine, diethylene tetraamine, triethylene tetraamine, tetraethylene pentamine, pentaethylene
30 hexamine, piperazine, aminoethylpiperzine, 1,4-Bis(3-aminopropyl)piperzine, N,N'-Bis(3-aminopropyl)ethylenediamine, 4,9-dioxa-1,12-dodecanediamine, 2,2'-(ethylenedioxy)bis(ethylamine), 4,7,10-trioxatridecane-1,13-diamine, 4,7-dioxadecane-1,10-
35 diamine, polyetheramine T 403, N,N-Bis (3-aminopropyl)-ethylene diamine, 3-2(2-aminoethyl)aminopropyl amine,

dipropyltriamine and 4,4'-diamino-dicyclohexylamine or combinations thereof.

Preferred adhesion promoters are amines such as 4,9-dioxa-1, 12-dodecane diamine, 4, 7, 10-trioxatridecane-1, 13-diamine and/or 4,7-dioxadecane-1, 10-diamine.

Preferred combinations of adhesion promoters include high and low molecular weight adhesion promoter combinations such as high and low molecular weight polyethylene imines and high and low molecular weight polyether glycols, for example, 4,9-dioxa-1, 12-dodecane diamine and polypropylene glycol.

The adhesion promoter(s) are generally present in an amount more than about 0.01%, preferably more than about 1%, more preferably up to about 10%, even more preferably up to about 50% and most preferably between about 1% and 50% based on the total weight of the activation treatment, or the combination of solvent(s), adhesion promoter(s) and any optional additives.

One or more additives known in the art of coatings may also be used in the method or activation treatment of the present invention. Suitable examples include rheology modifiers such as hydroxypropyl methyl cellulose (e.g. Dow, methocell 311), modified urea (e.g. Byk 411, 410) and polyhydroxycarboxylic acid amides (e.g. Byk 405); film formers such as esters of dicarboxylic acid (e.g. Lusolvan FBH, BASF) and glycol ethers (e.g. Dowanol, Dow); wetting agents such as fluorochemical surfactants (e.g. 3M Fluorad) and polyether modified poly-dimethyl-siloxane (e.g. Byk 307/333); surfactants such as fatty acid derivatives (e.g. Akzo, Bermadol SPS 2543) and quaternary ammonium salts; dispersants such as non-ionic surfactants based on primary alcohols (e.g. Merpol 4481, Dupont) and alkylphenol-formaldehyde-bisulfide condensates (e.g. Clariant 1494); substrate cling agents; anti foaming agents; anti corrosion reagents such as phosphate esters (e.g. ADD APT, Anticor C6), alkylammonium salt of (2-benzothiazolythio) succinic acid (e.g. CIBA, Irgacor 153)

and triazine dithiols; stabilizers such as benzimidazole derivatives (e.g. Bayer, Preventol BCM, biocidal film protection); levelling agents such as fluorocarbon-modified polymers (e.g. EFKA 3777); pigments such as
5 fluorescents (Royale Pigment and chemicals), and organic and inorganic dyes such as fluorescein.

The additives are usually present in an amount of less than about 10% based on the total weight of the activation treatment or the combination of solvent(s),
10 adhesion promoter(s) and additive(s).

The activation treatment may take different physical forms such as solution, suspension, mixture, aerosol, emulsion, paste or combination thereof. Treatments which take the form of a solution or emulsion are preferred.

15 The activation treatment may be prepared by mixing the components together with any mixing equipment known to those skilled in the art such as but not limited to stirrers, shakers, high speed mixers, internal mixers, extruders, mills, ultra-sound and gas dispersers. When
20 the activation treatment is in the form of a solution, the solution may be prepared as a concentrate and diluted before use or prepared ready for use.

The activation treatment or the application of the individual components thereof may be applied via any
25 method known to those skilled in the art such as but not limited to spray, brush, dip, knife, blade, hose, roller, wipe, pipette or combinations thereof. Application by spray is preferred.

The method of activation may be conducted at ambient
30 temperatures or alternatively at higher temperatures if desirable. The activation treatment or individual components thereof may be applied to small or large areas, to sections of larger parts, components or full infrastructure such as infrastructure associated with the
35 aerospace (e.g. aircraft), automotive (e.g. vehicles), marine (e.g. ships), transportation (e.g. trains), military (e.g. helicopter, missile) or construction

industries (e.g. buildings, factories, floors). The surface may have simple or complex geometry or may be at any inclination. Treatment may be conducted once or multiple times prior to interaction with the separate
5 entity. The exposure time of the activation treatment on the coating is more limited by the throughput and applications requirements. As such the exposure time may be short for example one minute or extended for example 3h.

10 In certain circumstances it may be preferable to remove excess non interlocked adhesion promoter and/or solvent from the surface. This process may be conveniently carried out by techniques such as solvent washing, wiping, air or gas knife and evaporation.

15 After the coating surface is activated, separate entities such as additional coating layers or coating details, adhesives sealants, stickers, and the like may be applied either immediately or at a later time, providing the surface remains predominantly uncontaminated during
20 storage or that the contamination can be conveniently removed. The activation solution may need to be reapplied in some cases.

Any suitable method known to those skilled in the art may be used to assess whether the adhesive linkage between
25 the organic coating and further coatings and/or other entities is fit for purpose. Such tests include but are not limited to ASTM, ISO, and FAA standards, in-house test methods to simulate in-service performance, in-service performance itself, and durability testing either actual
30 or accelerated. For the case of aerospace coatings, test methods based on water impact, such as the Whirling Arm Rain Erosion or the Single Impact Jet Apparatus (MIJA Limited, Cambridge, UK), have been found to be particularly useful for assessing inter-coat adhesion. In
35 this case, the amount of overcoat removal is related to the level of inter-coat adhesion.

BRIEF DESCRIPTION OF DRAWINGS

In the Examples, reference will be made to the accompanying drawings, in which:

Fig 1 is a schematic diagram showing the general
5 activation strategy; and

Fig 2 is a diagram showing whirling arm rain erosion performance assessment

EXAMPLES

10 The invention will now be described with reference to the following non-limiting examples. Although the examples concentrate on coatings derived from polyurethane chemistries it will be understood that the same activation methodology could be applied to coatings such as but not
15 limited to those based on epoxy, acrylic or polyester coatings through the appropriate choice of solvent(s), adhesion promoter(s) and optional additives under appropriate activation conditions.

- 20 1. Inter-coat adhesion of polyurethane paint as function of cure conditions/age
2. Effect of different solvent used in the surface activation treatment on inter-coat adhesion
3. Effect of different adhesion promoter used in the surface activation treatment on inter-coat adhesion
- 25 4. Effect of different adhesion promoter concentration used in the surface activation treatment on inter-coat adhesion
5. Effect of surface activation treatment time on inter-coat adhesion
- 30 6. Effect of substrate inclination (angle) on application of the surface activation treatment and resultant inter-coat adhesion
7. Effect of additives used in the surface activation treatment on inter-coat adhesion
- 35 8. Effect of dwell time between activation and re-coating on inter-coat adhesion

9. Impact of different application methods for applying the activation treatment on the resultant inter-coat adhesion

10. Impact of different post treatment steps to
5 remove excess treatment and /or solvent on the resultant inter-coat adhesion

11. Effect of different paint types and curatives on the activation treatment and resultant inter-coat adhesion

12. Durability of coatings applied to activated
10 substrates

13. Inter-coat adhesion between aged and then activated organically pigmented coating towards an additional coating layer

14. Adhesion data from Whirling Arm Rain Erosion and
15 SIJA experiments of activated and re-coated specimens relative to specimens sanded prior to over-coating

15. SEM analysis of coating layers

16. Raman Spectroscopy illustrating activation solution penetration depth

17. Analysis of coating surface by XPS prior to and
20 following activation

All the components of the activation treatment influence the physical properties of the treatment and
25 hence its ability to interact with the coating. Such impacts can be assessed theoretically by using solubility parameters (Hanson, Hanson solubility Parameters - a users hand book, CRC, NY, Van Krevelen, D.W., Hoftyzer, P.J., Properties of Polymers - their estimation and
30 correlation with chemical structure, Elsevier, NY) or UNIFAC (Hansen H.K., et al. Ind. Eng. Chem. Res 1991; 30 (10) p2352) to estimate the contribution of the individual components to the total interaction parameter of the activation treatment.

35 It is envisaged that suitable combinations of components of the activation treatment will differ depending on the type of coating to be activated. The

appropriate choice of solvent(s), adhesion provider(s), optional additives and activation conditions will differ depending on the type of coating to be activated.

5 General Experimental Detail:

1. Aluminium Pre-Treatment

Aluminium test coupons (2024-T3) or Rain erosion Foils (Alclad 2024-T3) were cleaned and an Alodine type conversion coating was applied prior to painting.

2. Painting Conditions and Protocol

An epoxy based primer was used for all samples. Desothane polyurethane topcoats were employed for all trials using the standard flow control agent (CA 8000C) unless specified. The base CA8000 : activator CA8000B : flow CA8000C ratio employed was also calculated on a weight basis (121.06 : 51.32 : 39.81 for white 7067) unless stated in the example. Following component addition, both primer and topcoats were shaken for 15 min in a "Red Devil" paint shaker and allowed to stand for a further 15 min prior to painting.

Spray painting of flat panels was carried out employing a robotic painting arm incorporating a gravity fed automatic spray gun. Spray painting was conducted using an inlet pressure of 40 PSI, a scan rate of 100 mm/s and a specimen to gun distance of 300 mm. A single pass was employed for the application of the primer whilst four individual passes were required for the top-coats allowing "tack-up" time between each individual pass. The coating thickness was controlled by the gun's fluid needle control position and scan rate with these adjusted in line with paint thickness measurements assessed using a Fischer Isoscope (MPOD). An analogous strategy was employed for the application of the overcoat, Desothane HS polyurethane. For the majority of the research the painted films were over-coated following taping of the top

and bottom of the coupons with vinyl tape to form a leading paint edge on its removal. This edge was the impact target for SIJA analysis. Later investigations applied the tape through the middle of the coupon.

5

Table 2 Painting & Cure Schedule

Task	Conditions
Polyurethane Top-coat	Conducted on the same day as the primer Cure: 18 h, 49°C, 10-22% relative humidity, Thickness ~100 micron (measured each batch)
Surface modification and/or analysis	Generally conducted directly following completion of the cure cycle or on the following day
Polyurethane over-coat repainting	Painting conducted on the same or next day following treatment. Cure: 40h, 49°C, 10 - 22% relative humidity, Thickness ~100 micron (measured each batch)

10 Spray painting of curved surfaces (eg: rain erosion
foils) was conducted using a Binks M1-H HVLP gun
configured with a 94 nozzle. In these cases the aluminium
was prepared in the same manner as the SIJA plates prior
to the first top-coat being applied. Following cure of
the first coating layer the front of the foils were masked
15 prior to over-coating to form a leading edge once the
over-coating was applied and tape removed.

3. Surface Modification

20 The solvents and reagents used for surface
modification were purchased from the MERK and Sigma-
Aldrich Chemical Companies of an Analytical and Laboratory
Reagent grade purity respectively. The specific adhesion
promoter or solvent employed for activation is outlined in
the main body of the example.

25 General treatment conditions are presented in Table
3. Activation of the 'aged' painted surfaces was
conducted either on the same day or next day following
completion of curing unless stated in the example.

Table 3 General Activation Protocol

Task	Strategy
Treatment	<p>Coupons were placed:</p> <ul style="list-style-type: none"> • Horizontally over a grid and then exposed to the treatment solution from 5 to 180 min, either periodically re-applying the solution or with just one application. • At angles of 0, 45, 90, 135° and then exposed to a treatment solution spray at 10 min intervals for 30 min or with one application.
Post-Treatment	<ul style="list-style-type: none"> • Washed with isopropanol • Wiped with an isopropanol soaked cloth • Used directly for painting
Re-coating	<p>Coupons were either painted on the :</p> <ul style="list-style-type: none"> • Following Day (24 h) • Same day (5 min to 4 hours after treatment)

5 Application was conducted either by pouring treatment solution over the substrate with a pipette, application with a disposable pump action spray bottle or by using a Binks M1-H HVLP gun employing a 92 or 94 nozzle and 40 psi inlet pressure.

10

4. Analysis

Table 4 provides the equipment and conditions used for polyurethane surface analysis and adhesion testing.

15 Table 4 Analytical Equipment & Conditions

Equipment	Conditions
FTIR	FTIR analysis was carried out on a BRUKER FTIR/NIR spectrometer or Nicolet Instruments employing an ATR KRS-5 TiBr / TiI mixed crystal associated with the microscope
Raman Spectroscopy	Raman spectroscopy was completed on a Renishaw, 1000 Raman microprobe spectrometer employing a 780 nm laser, focusing the laser spot down to 1 micron. Cross sections of the painted films on glass, or aluminium were prepared by cutting the paint film and exposing the cross section to the incident laser beam.

Table 4 Analytical Equipment & Conditions cont.

XPS	XPS analysis was completed on a Kartos AXISH5 spectrometer at an incident beam of 90° employing an Alumina source to generate survey and high resolution spectra. Curve fitting analysis of the data was completed using GRAMMS RESEARCH software package												
Contact Angle	Contact angle analysis was completed using “FIRST TEN ANGSTROMS” semi-automated video equipped contact angle analyser. CH ₂ I ₂ and H ₂ O were employed as the reference solvents to calculate the dispersive (γ_s^d) and polar (γ_s^p) contributions to surface energy (γ_s) through the Young-Dupre relationship and Fowkes equation.												
SEM	SEM analysis of the polyurethane cross-sections were collected on a Oxford Pentafet detector controlled by an Oxford ISIS system. Cross-sections of the samples prepared with a cut off saw appropriate for non-ferrous materials and were mounted in epoxy resin, ground and polished to a 1 micron finish and gold coated. Imaging and x-ray analysis was conducted using a 15 KV accelerating voltage and a 17 mm working distance. EDX analysis was specifically refined for carbon, nitrogen, oxygen, and chlorine.												
SIJA	Adhesion testing was completed using a Single Impact Jet Apparatus (SIJA) manufactured by MIJA, Ltd in Cambridge, UK. The initial equipment was configured using a 0.8 mm nozzle and employed 0.22 calibre 5.5 mm Crosman Accupell Pointed Pellets (#11246). Testing was completed following immersion in water for 16 to 18h employing a line laser to locate the impact position and using a 45° specimen to impact droplet geometry. A single water jet was employed at each site to test adhesion with the pressure employed for the “shot” indicated below its impact. The velocity of each individual shot was recorded for future reference, but generally the pressure to velocity conversion is specified below (± 25 m/s).												
	<table><tr><th>Pressure (PSI)</th><th>Velocity (m/s ± 25 m/s)</th></tr><tr><td>L</td><td>350</td></tr><tr><td>100</td><td>725</td></tr><tr><td>200</td><td>895</td></tr><tr><td>300</td><td>1007</td></tr><tr><td>400</td><td>1079</td></tr></table>	Pressure (PSI)	Velocity (m/s ± 25 m/s)	L	350	100	725	200	895	300	1007	400	1079
	Pressure (PSI)	Velocity (m/s ± 25 m/s)											
L	350												
100	725												
200	895												
300	1007												
400	1079												
	In some cases the amount of overcoat removed, and hence the inter-coat adhesion was assessed employing image analysis techniques to quantify the area of paint removed. More overcoat removed corresponded with inferior inter-coat adhesion												

Table 4 Analytical Equipment & Conditions cont.

Whirling Arm Rain Erosion Testing	<p>Rain erosion testing was completed on a whirling arm rain erosion apparatus employing a 52 inch zero lift helicopter like propeller run at 3600 rpm. Reference and activated polyurethane topcoat foils were over-coated (60 to 100 micron paint thickness) following masking to produce a leading edge. The foils were attached to the propeller at a distance along the propeller correlating to a velocity of 380 mile per hour at the mid point of the foil. The effective rain field density of 2 mm droplets used during the experiment was 1 inch per hour. After 30 min the impact of rain erosion on the inter-coat adhesion of the foils was evaluated according to a 0.5 to 5 rating correlating the amount of paint removed or tear lengths (see figure 2). The impact of water droplets on the leading edge of the over-coat formed on removal of the tape during the experiment erodes the over-coating layer relative to the strength of the inter-coat adhesion.</p>
--	---

Inter-coat adhesion of white polyurethane painted specimens cured under various conditions prior to over-coating with blue polyurethane as assessed by SIJA:

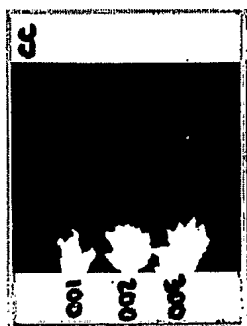
- 10



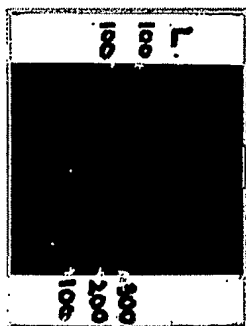
20

Inter-coat adhesion as assessed by SIJA of white polyurethane paint cured at 49°C for 18 h and then treated with the adhesion promoter specified in different solvents prior to over-coating with blue polyurethane.

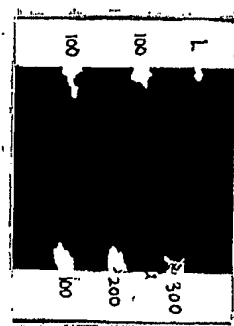
1. Chlorinated Solvents (amine terminated polypropylene glycol adhesion promoter)



Untreated

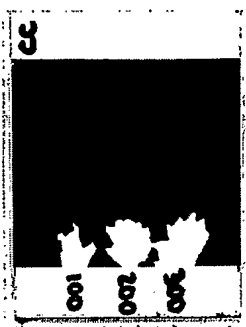


Dichloromethane

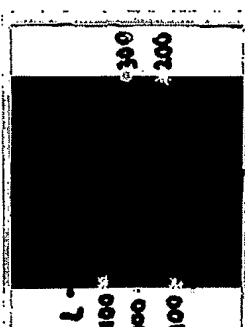


Dichloroethylene

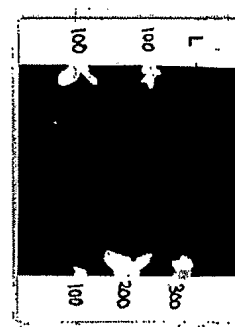
5 2. Alcohol solvents (amine terminated polypropylene glycol adhesion promoter)



Untreated

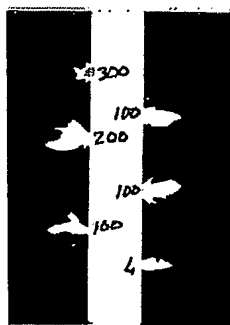


Benzyl alcohol

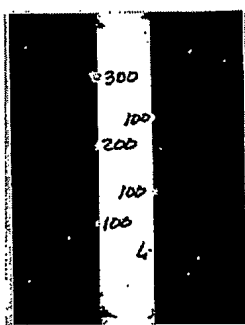


Ethylene glycol
monomethyl ether

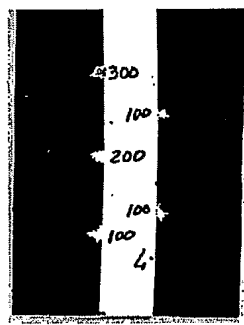
10 3. Ester Solvents (4,7,10-trioxa-1,13-tridecanediamine adhesion promoter)



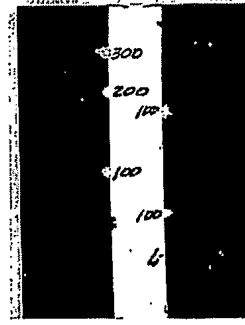
Untreated



ethyl acetate

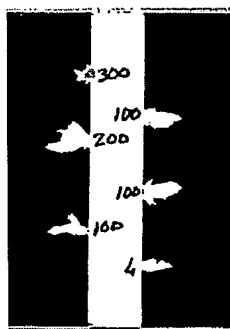


t-butyl acetate

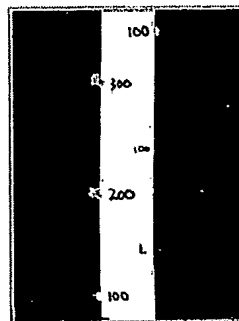


i-propyl acetate

4. **Ketone Solvents** (4,7,10-trioxa-1,13-tridecanediamine adhesion promoter)

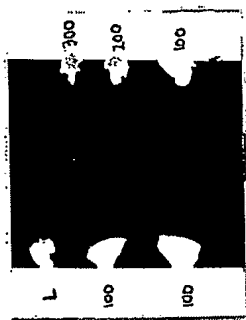


Untreated

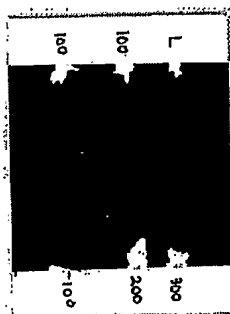


methyl amyl ketone

5. **Ether Solvents** (4,7,10-trioxa-1,13-tridecanediamine adhesion promoter)



Untreated

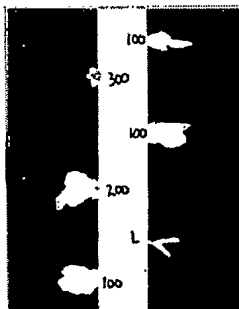


ethylene glycol
dimethyl ether

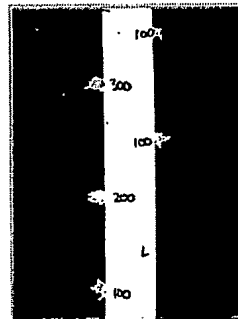


tetrahydrofuran

10 6. **Amide Solvents** (4,7,10-trioxa-1,13-tridecanediamine adhesion promoter)

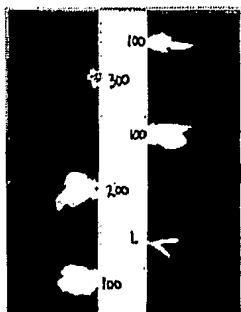


Untreated

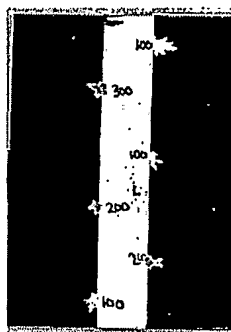


N-methyl pyrrolidinone

7. Solvent mixtures

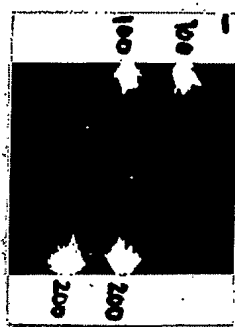


Untreated



N-methyl Pyrrolidinone : Ethyl acetate (1:1) 4,7,10-trioxa-1,13-tridecanediamine

5



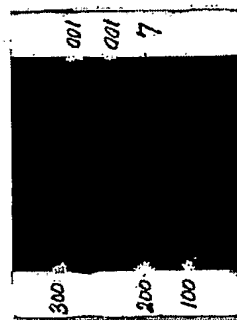
Untreated



Dichloromethane : Benzyl alcohol (1:1) amino terminated polypropylene glycol

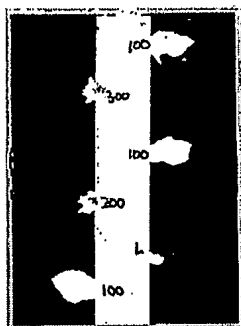


Untreated

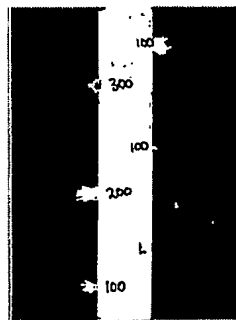


Ethyl acetate : Benzyl alcohol (1:1) 4,7,10-trioxa-1,13-tridecanediamine

10



Untreated



Ethyl acetate : diglycol
ether dimethyl ether (1: 1)
4,7,10-trioxa-1,13-
tridecanediamine

5

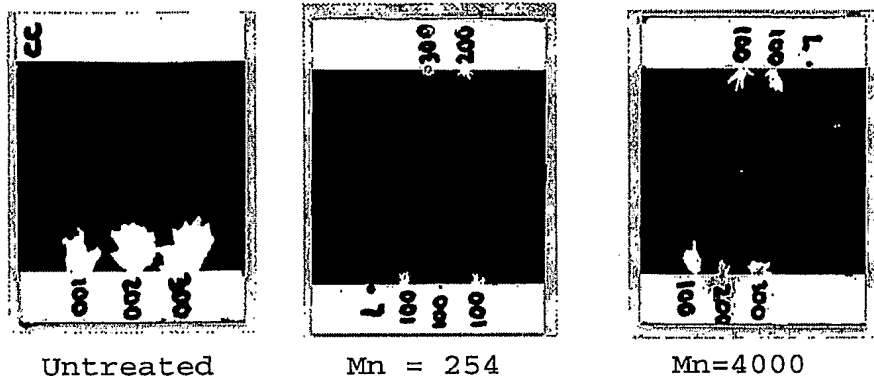
Results indicate:

Chemical activation of polyurethane may be conducted
with suitable adhesion promoters in a variety of different
10 solvents or solvent combinations to improve inter-coat
adhesion relative to samples which are not activated prior
to over-coating.

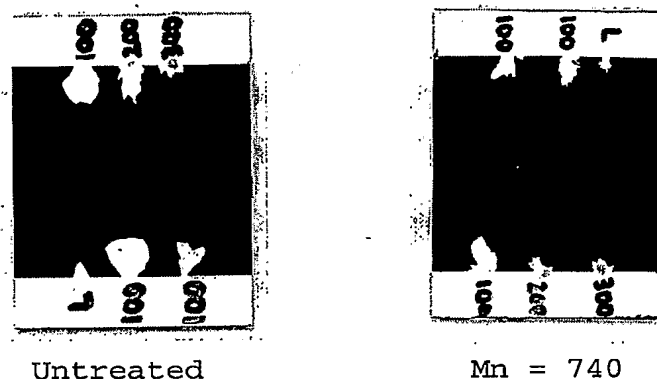
Example 3

15 The following example show the improvement in inter-
coat adhesion of aged polyurethane white coatings (18h,
49°C) treated with various adhesion promoters (50%)
employing ethyl acetate or benzyl alcohol as the treatment
solvent prior to over-coating with blue polyurethane as
20 assessed by SIJA analysis. (Treatment time 30 or 60 min)

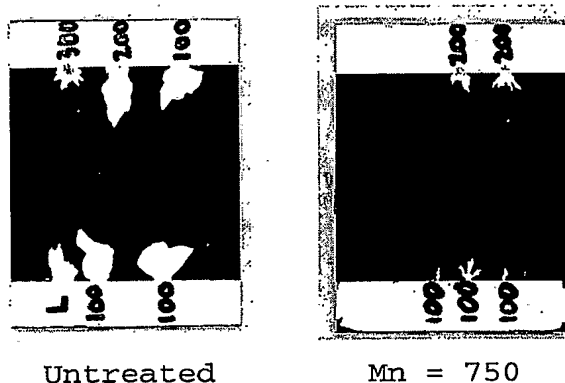
1. Amine terminated polypropylene glycol (Benzyl alcohol)



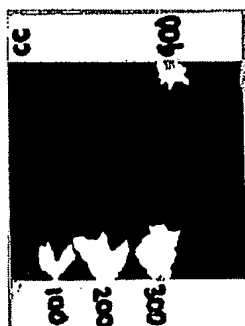
2. Alcohol terminated polypropylene glycol (Benzyl alcohol)



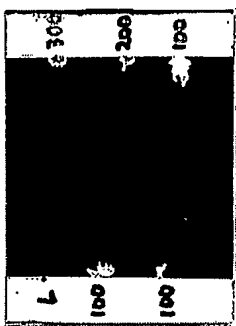
3. Epoxy terminated polypropylene glycol (benzyl alcohol)



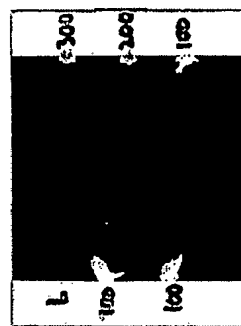
4. Polyethylene imine (PEI) (ethyl acetate)



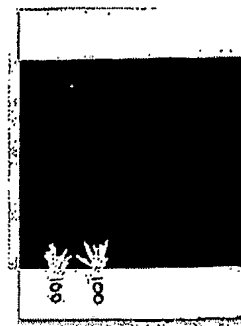
Untreated



Linear
(Mw 425)

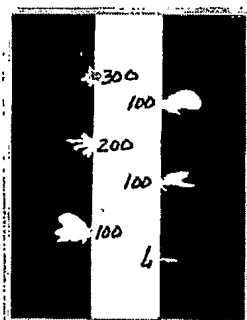


Branched
(Mw=800)

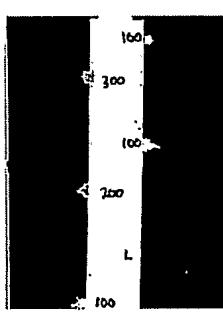


Branched
(Mw=25000)

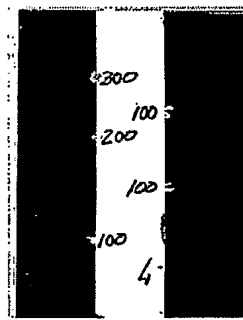
5. Amine functional ether compounds (ethyl acetate)



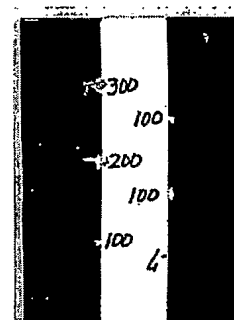
Untreated



4,7,10-trioxa-
1,13-
tridecanediamine



4,9-dioxadodecane
-1,12-diamine



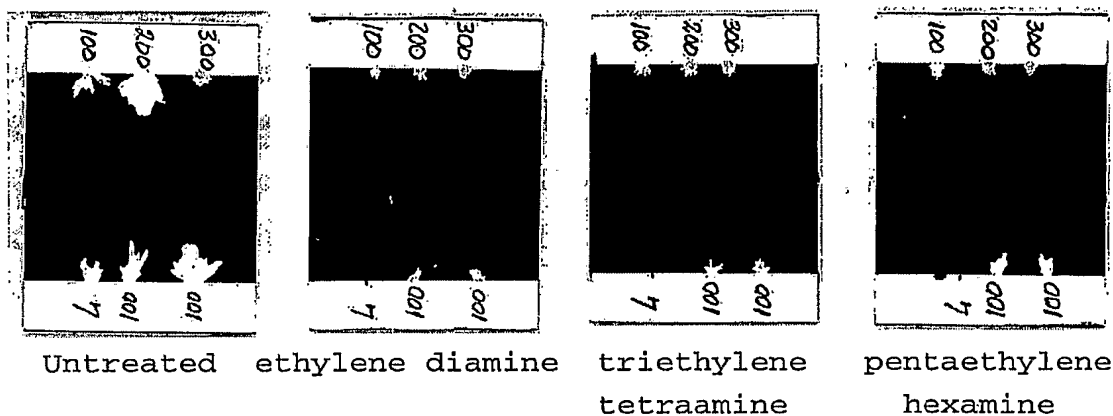
4,7-dioxadecane-
1,10-diamine

10

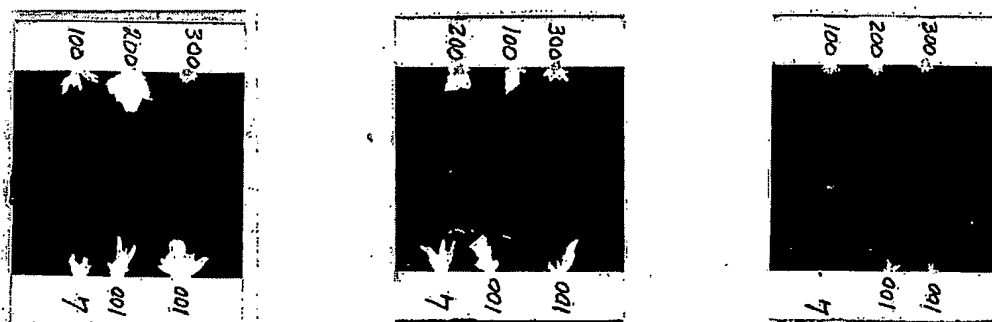
15

20

6. Amine functional compounds (ethyl acetate)



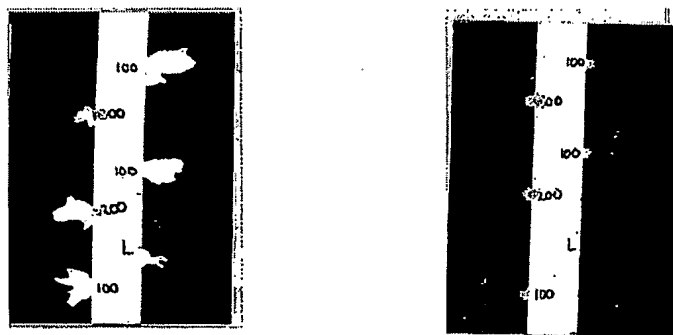
5 7. Impact of employing a mono-functional adhesion promoter on inter-coat adhesion (benzyl alcohol)



(PEI - polyethylene imine linear MW=425)

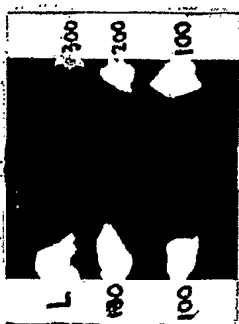
8. Impact of employing adhesion promoter combinations on adhesion (ethyl acetate)

10

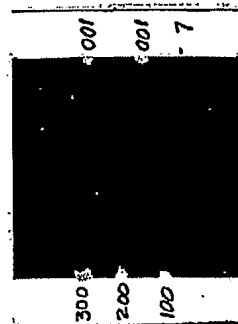


Untreated

PEI (branched MW 25K), 10% &
PEI linear 0.43K 50%



Untreated



4,7,10-trioxa-1,13-tridecanediamine
(40%), diethylene triamine (10%) in
benzyl alcohol

5

Results indicate:

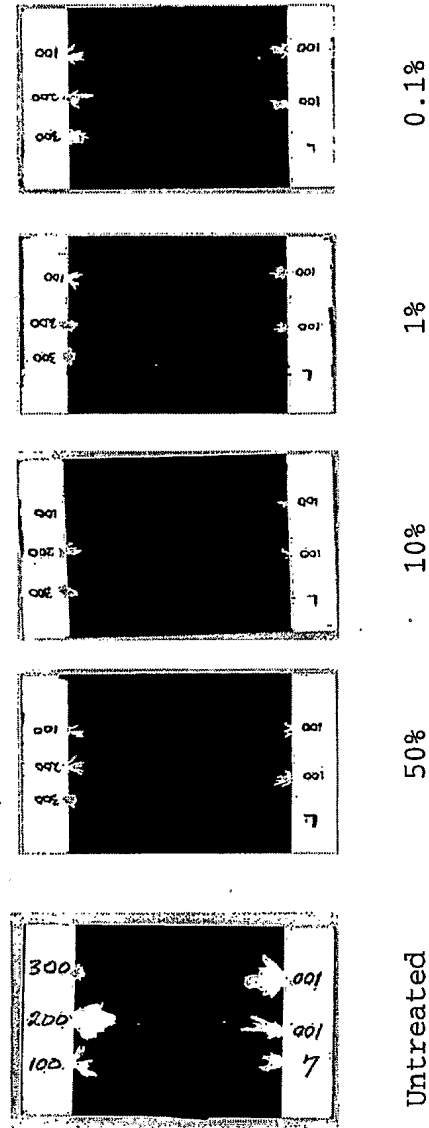
A variety of different suitably functionalised adhesion promoters or adhesion promoter combinations may be employed to improve inter-coat adhesion including those which are polymeric or discrete molecules. Example 3 (7) illustrates that inter-coat adhesion is slightly improved through the use of monofunctional adhesion promoters such as propyl amine, due to the similar amount of over-coat paint removal compared with untreated samples.

15

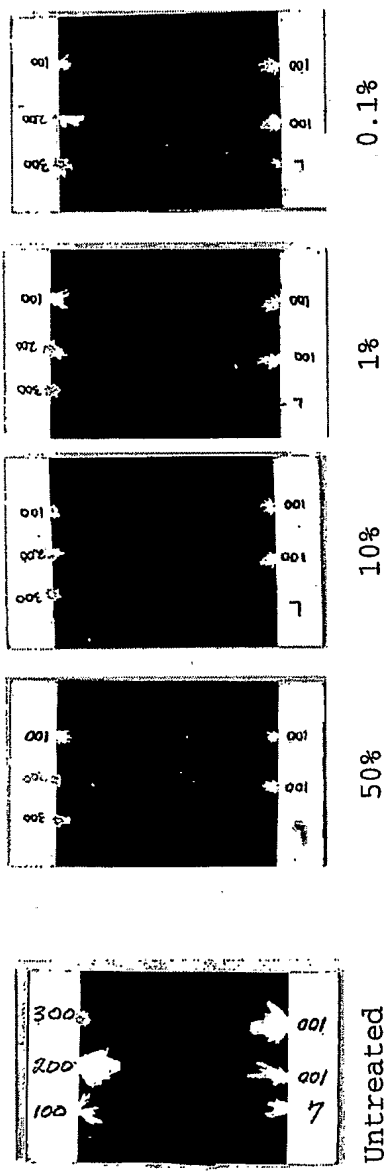
Example 4

The following example shows the effect of using various adhesion promoter concentrations to improve the inter-coat adhesion of aged polyurethane topcoat (49°C, 18h) to a blue polyurethane over-coat as assessed by SIJA analysis.

1. PEI (linear) in ethyl acetate, 30 min treatment time



2. 4,7,10-trioxa-1,13-tridecanediamine in ethyl acetate, 30 min



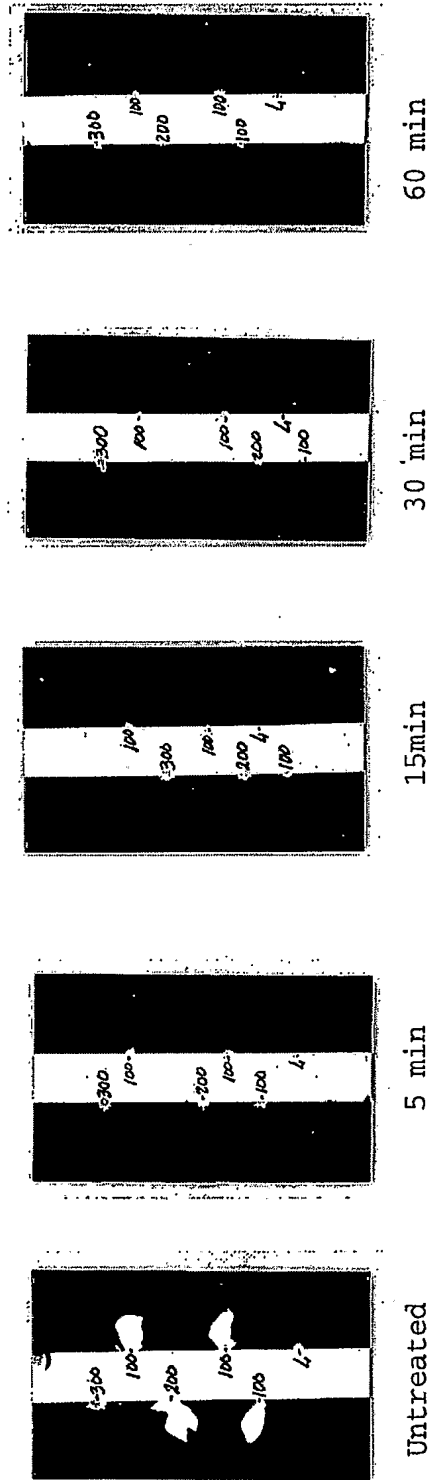
Results indicate:

When appropriate adhesion promoter and solvent are employed, the adhesion promoter concentration may be varied whilst still providing an improvement in inter-coat adhesion.

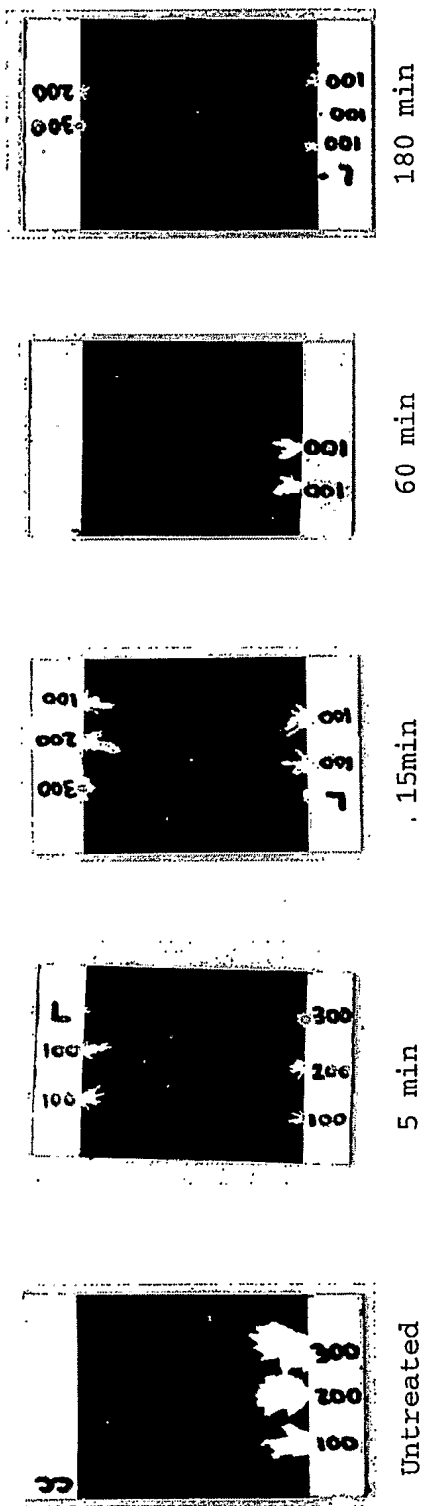
Example 5

The following example illustrates the effect on inter-coat adhesion of treating aged white polyurethane coating (18 h, 49°C) with an activation solution for different time periods prior to over-coating with blue polyurethane coating as assessed by SIJA analysis.

1. 4,7,10-trioxa-1,13-tridecanediamine (50%) in Ethyl acetate



2. Amino-terminated Polypropylene glycol (Mn = 230) in Benzyl alcohol



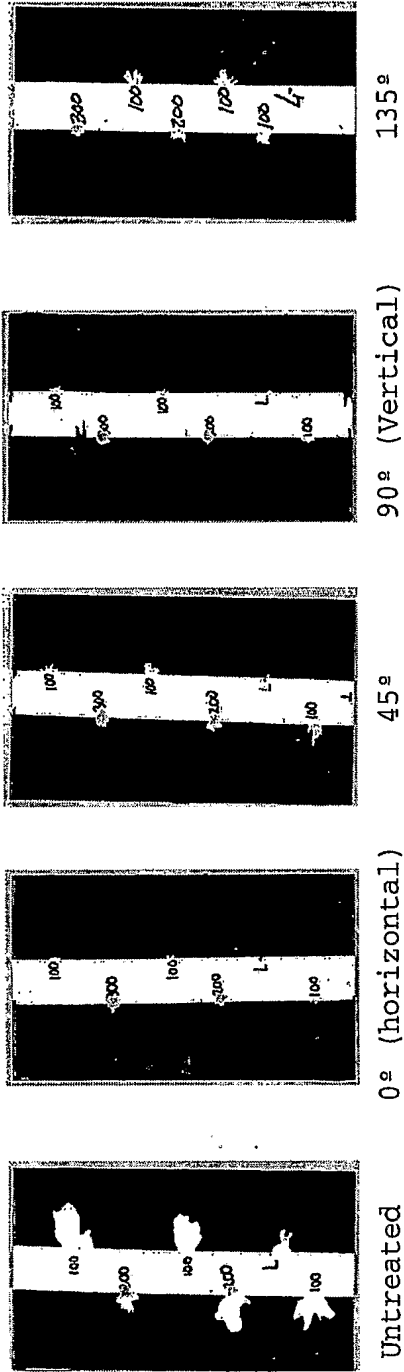
Results indicate:

The SIJA results indicate that when suitable adhesion promoters and solvents are employed the activation process may be conducted over short or extended periods to improve inter-coat adhesion.

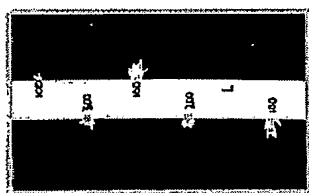
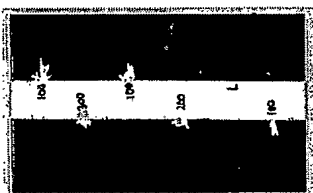
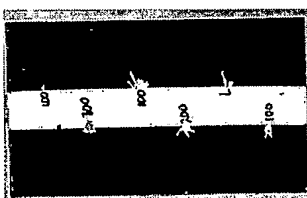
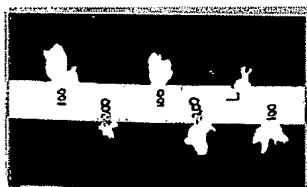
Example 6

Example 6 shows the effect on inter-coat adhesion as assessed by SIJA analysis of aged white polyurethane coating (49°C, 18h) activated with suitable adhesion promoters and solvents prior to over-coating with blue polyurethane coating at different inclinations.

A. 4,7,10-trioxa-1,13-tridecanediamine (50%) in ethyl acetate. (30 min treatment time)



2. PEI Linear (50%) in benzyl alcohol (60 min treatment time)



Untreated

0° (horizontal)

45°

90° (Vertical)

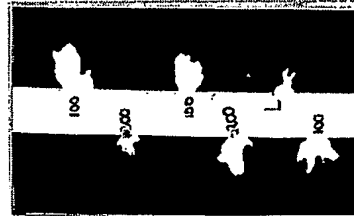
Results Indicate:

When suitable adhesion promoters and solvents are employed the activation treatment may be used to improve inter-coat adhesion of aged polyurethane substrates at different inclinations and hence is suitable for substrates of different geometries.

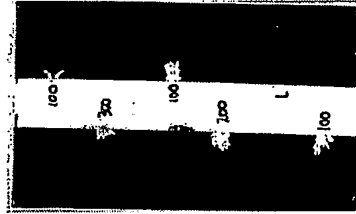
Example 7

The following example illustrates the effect of including minor amounts of additives (in this case shear thinning rheology modifiers) in the activation treatment solution. In this case an aged polyurethane white coating (49°C, 18 h) was treated with the activation solution prior to over-coating with a blue polyurethane coating and the inter-coat adhesion assessed by SIJA.

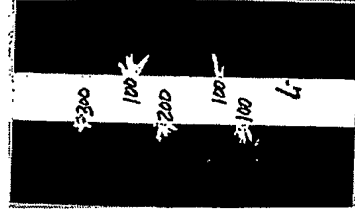
A. 10% Polyethylene imine (linear) in ethyl acetate, substrate at 45° incline (30 min treatment time)



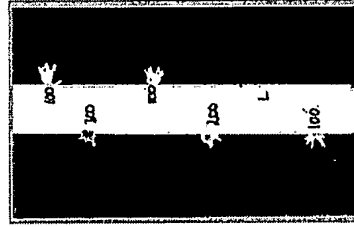
Untreated



No additive

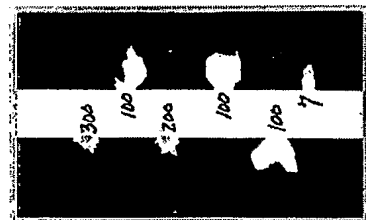


1% Methocell

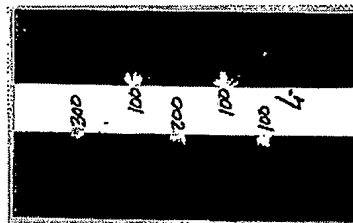


1% Crayvallac

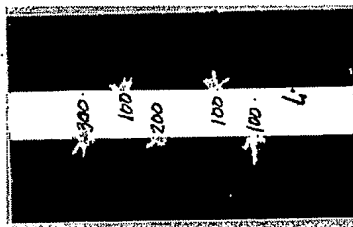
B. 4,7,10-trioxa-1,13-tridecanediamine (%) in Ethyl acetate substrate at 90°
incline (30 min treatment time)



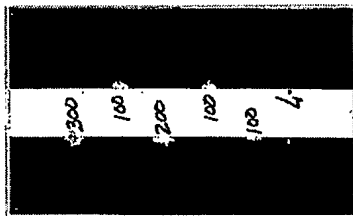
Untreated



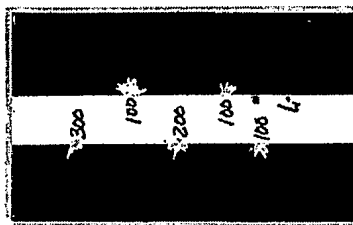
50%



1%



50% + 0.5%
Methocell



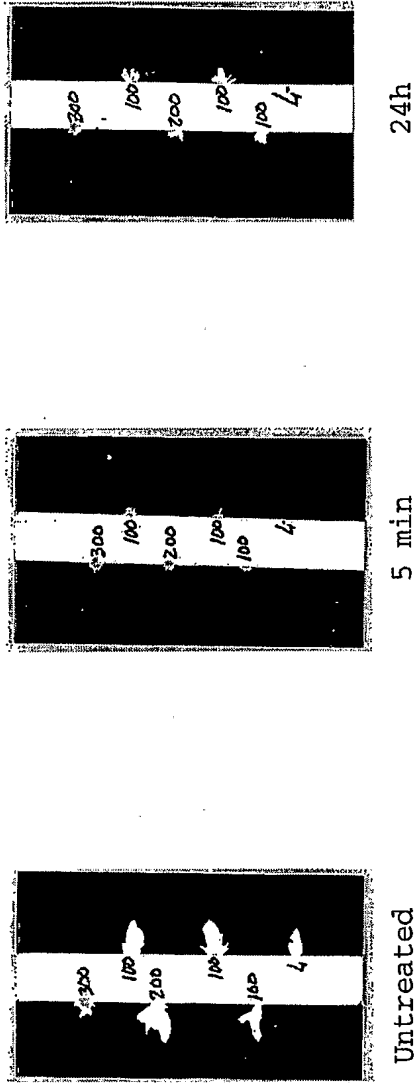
1% + 0.5%
Methocell

Results indicate:

Additives such as but not limited to rheology modifiers may be added into the activation solution without detrimental impact on the level of inter-coat adhesion improvement as assessed by SIJA techniques. In this case such modifiers limit the amount of activation solution run off during the activation procedure.

Example 8

Example 8 illustrates the effect of different dwell times between activating the surface of the aged white polyurethane coating (18h, 49°C) and over-coating with fresh blue polyurethane employing 4,7,10-trioxa-1,13-tridecanediamine (50% in ethyl acetate, 30 min) as the activation solution.

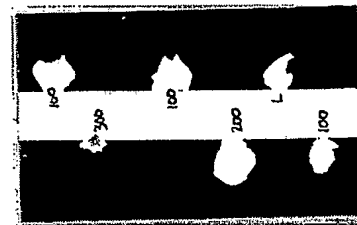


Results indicate:

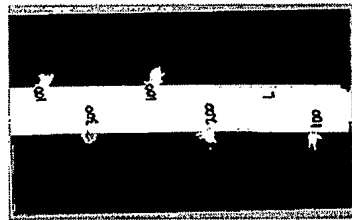
Specimens may be over-coated employing either a short or longer dwell time between activation and over-coating. As long as the specimens are stored appropriately an improved inter-coat adhesion results as assessed by SIJA methods..

Example 9

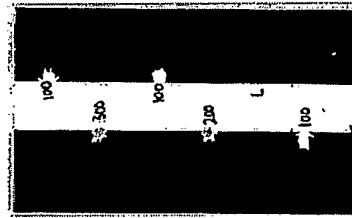
Example 9 shows the impact on inter-coat adhesion of applying the activation solution to the aged white polyurethane coating (49°C, 18h) by different techniques. Treatment conducted at a 45o angle (4,7,10-trioxa-1,13-tridecanediamine 50% in ethyl acetate, 30 min) prior to over-coating with blue polyurethane.



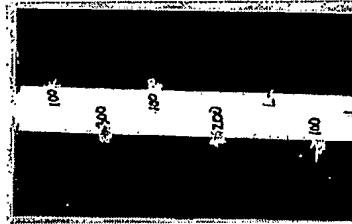
Untreated



HVLV Spray Gun



Mechanical Spray Bottle



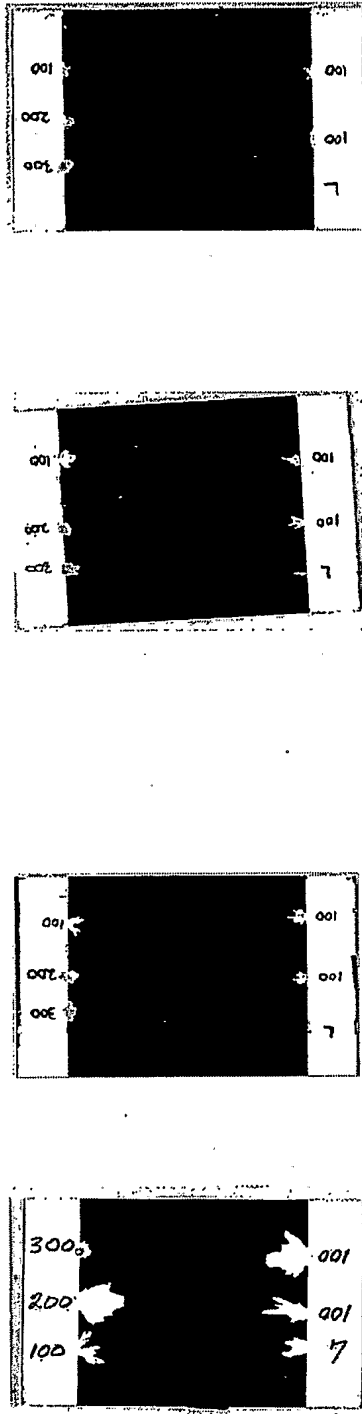
Pipette

Results indicate:

Improved inter-coat adhesion results as assessed by SIJA techniques regardless of the application method employed.

Example 10

Example 10 shows the effect of various post treatment protocols employed following treatment of the aged white coating (49°C, 18 h) with the activation solution (1 % 4,7,10-trioxa-1,13-tridecanediamine in ethyl acetate) prior to over-coating with blue polyurethane.



Untreated isopropyl alcohol wash isopropyl alcohol wipe no wipe or wash

Results indicate:

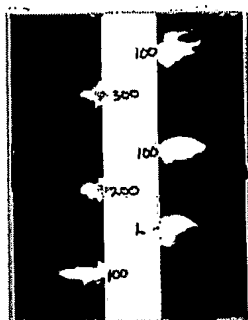
Chemical activation treatment is amenable to a variety of different post treatment steps if required for example those to removed excess adhesion promoter, solvent or contaminant whilst retaining an improved level of inter-coat adhesion as assessed by SIJA analysis

Example 11

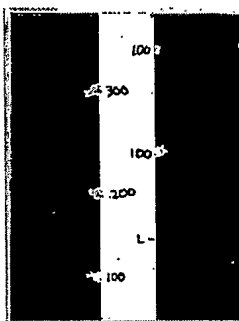
The following example shows how the appropriate adhesion promoters such as 4,7,10-trioxa-1,13-tridecanediamine and solvents (eg ethyl acetate) may be used to improve inter-coat adhesion of aged (49°C, 18 h) :

- a. polyurethane coatings manufactured by different paint manufacturers and
- b. polyurethane coatings cured with hot thinners (ie thinners incorporating higher level of cure catalyst) prior to over-coating with blue polyurethane

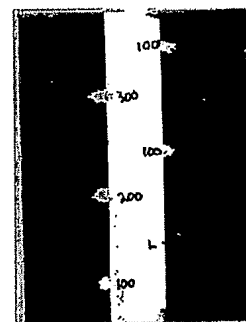
A1. Desothane HS Paint Range (PPG Aerospace PRC Desoto)



Untreated



50%

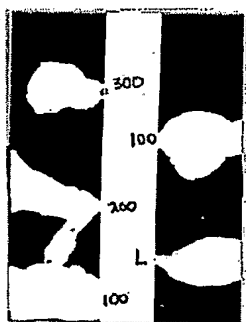


1%

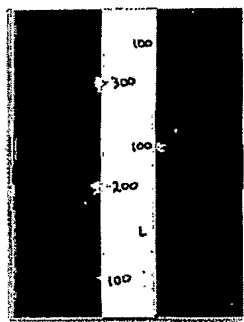
4,7,10-trioxa-1,13-tridecanediamine

15

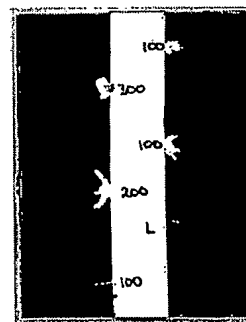
A2. Eclipse Range (Akzo Nobel Aerospace Coatings)



Untreated



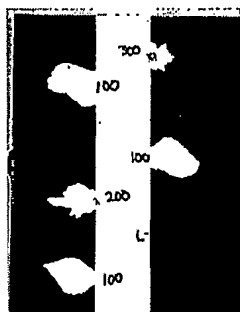
50%



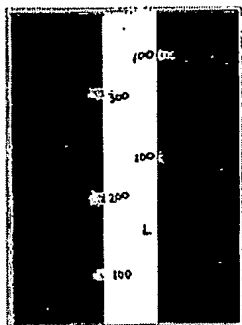
1%

4,7,10-trioxa-1,13-tridecanediamine

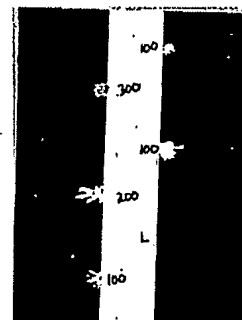
B. Desothane HS cured with hot thinners



Untreated



50%



1%

4,7,10-trioxa-1,13-tridecanediamine

5 Results indicate:

The activation procedure is amenable for improving the adhesion between different types of polyurethane coatings and coating cured with different thinners (catalyst levels) and hence different cure rates and fresh coating layers as assessed by SIJA analysis.

Example 12

The following example illustrates that the activation procedure may be:

- 15 A. Carried out on aged coatings, that
- B. Under appropriate storage conditions the activated surface is durable, that
- C. Inter-coat adhesion is durable over time and that
- 20 D. Inter-coat adhesion is resistant to chemical exposure

A. Inter-coat adhesion of aged coatings prior to over-coating

- 5 (1) White coating aged for 156 h, 49°C prior to over-coating with Blue coating

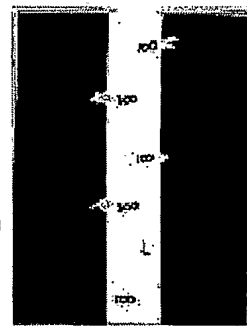
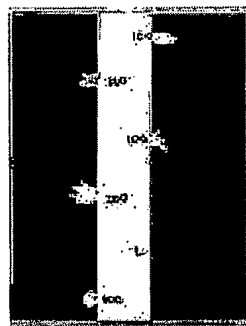
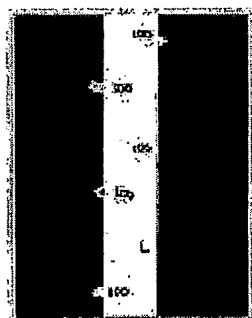
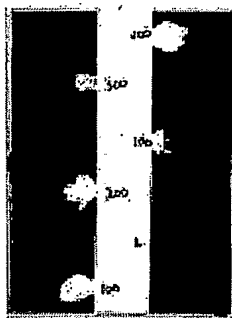


Untreated



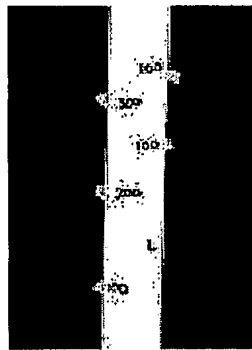
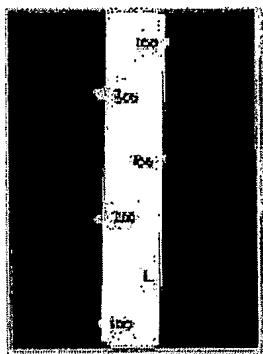
Treatment : Amino-terminated polypropyleneglycol 50% in dichloromethane (30 min)

- 10 (2) White topcoats cured for 16 h, 49°C and stored for 3 months under ambient conditions prior to over-coating with blue polyurethane coating (treatment: 50% adhesion promoter in ethyl acetate, 30 min)



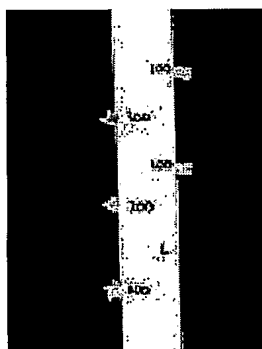
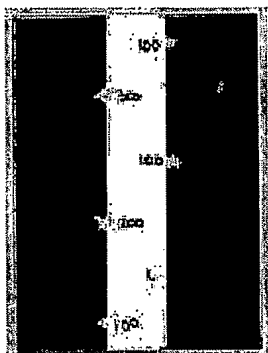
15 Untreated 4,7,10-trioxo-1, Polyethylene- Triethylene
13-tridecanediamine imine (1) tetraamine

B. Inter-coat adhesion of aged activated surface. (Aged white polyurethane coatings (49°C, 18 h), activated, and stored under ambient conditions for three months prior to over-coating with blue polyurethane)



(Treatment 50%
4,7,10-trioxa-1,13-
tridecanediamine in
ethyl acetate,
30 min)

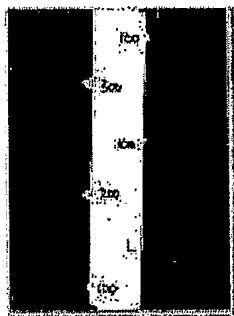
5 Original Adhesion Adhesion after 3 month ambient
storage prior to over-coating



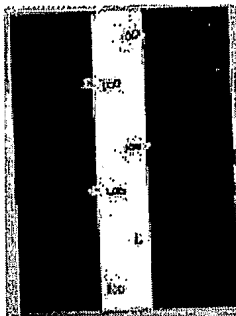
(Treatment 50%
Polyethylene imine
(linear) in ethyl
acetate, 30 min)

10 Original Adhesion Adhesion after 3 month ambient
storage prior to over-coating

C. Inter-coat adhesion over time. (Activation of aged white polyurethane coatings (49°C, 18 h) prior to over-coating with blue polyurethane)

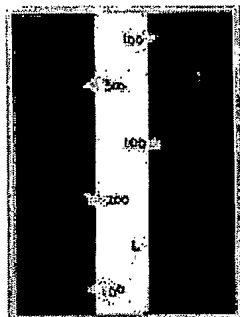


5 Adhesion 2 days

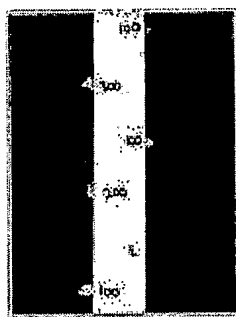


Adhesion after
5 month ambient storage

(Treatment 50%
4,7,10-trioxa-1,13-
tridecanediamine in
ethyl acetate,
30 min)



Adhesion 2 Days

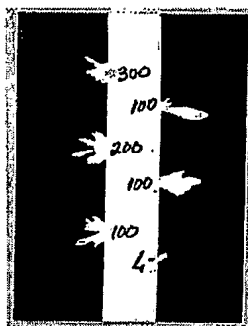


Adhesion after
5 months ambient storage

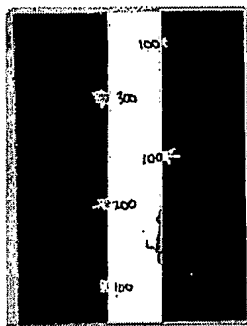
(Treatment 50%
Polyethylenen imine
(linear) in ethyl
acetate,
30 min)

D. Following exposure to Skydrol Hydraulic Fluid for 30 days

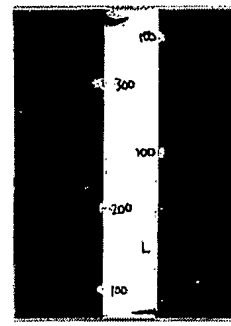
No Exposure



5 Untreated

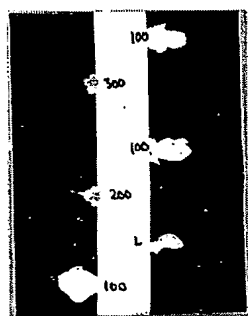


Polyethylene imine
(linear)

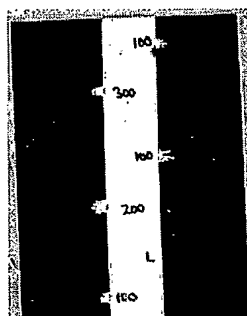


4,7,10-trioxa-1,13-
tridecanediamine

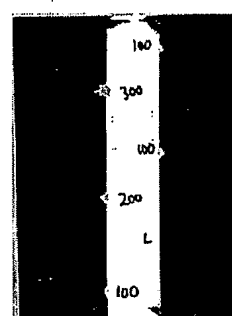
30 day exposure



10 Untreated



Polyethylene imine
(linear)



4,7,10-trioxa-1,13-
tridecanediamine

(treatment 50% adhesion promoter in ethyl acetate)

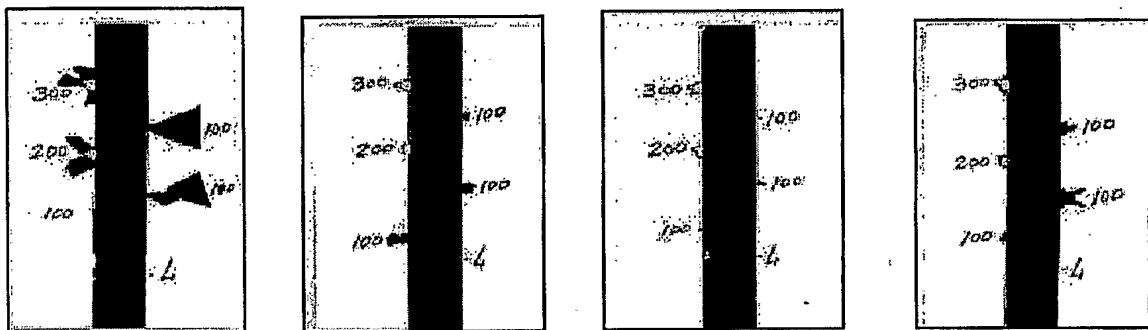
Results indicate:

- 15 Polyurethane coatings aged for extended periods under
ambient or higher temperatures may be activated by
application of the activation treatment to produce
improved inter-coat adhesion as assessed by SIJA
techniques. The activated surface itself is also robust
20 under appropriate storage conditions, as is the inter-coat
adhesion between paint layers over time as well as

following exposure to chemicals such as those used in hydraulic fluid.

Example 13

- 5 The following example illustrates the inter-coat adhesion between aged and then activated organically pigmented polyurethane coating (blue) towards an additional coating layer (white).



- 10 Untreated 4,7,10-trioxa-1,13-tridecanediamine 4,7-dioxadecane-1, 10-diamine triethylene tetraamine

Treatment 50% adhesion promoter in ethyl acetate, 30 min.

15

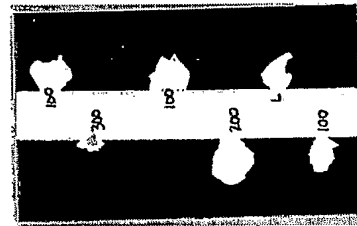
Results indicate:

- 20 The adhesion promoting treatment provides improved inter-coat adhesion between aged organically pigmented coating (eg blue) and additional coating layers.

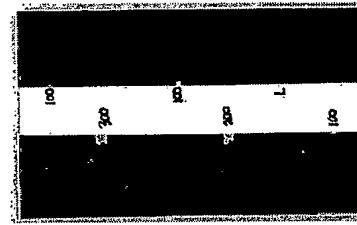
Example 14

The following example indicates that the inter-coat adhesion produced through chemical activation with suitable adhesion promoter/s and solvent/s is comparable to that produced by sanding and as such it may be used to replace the sanding process as a mechanism of improving the adhesion of coatings which are aged to fresh coating layers.

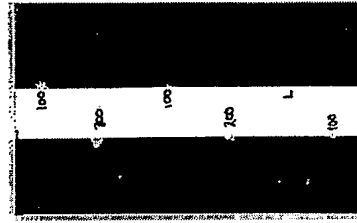
A. SIJA inter-coat adhesion of aged polyurethane coatings (49°C, 18h) which were then over-coated with blue polyurethane top-coat (activation solution 50% adhesion promoter in ethyl acetate)



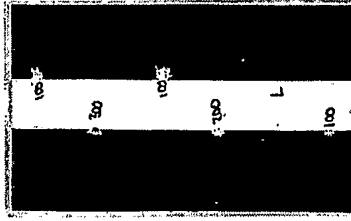
Untreated



Sanded

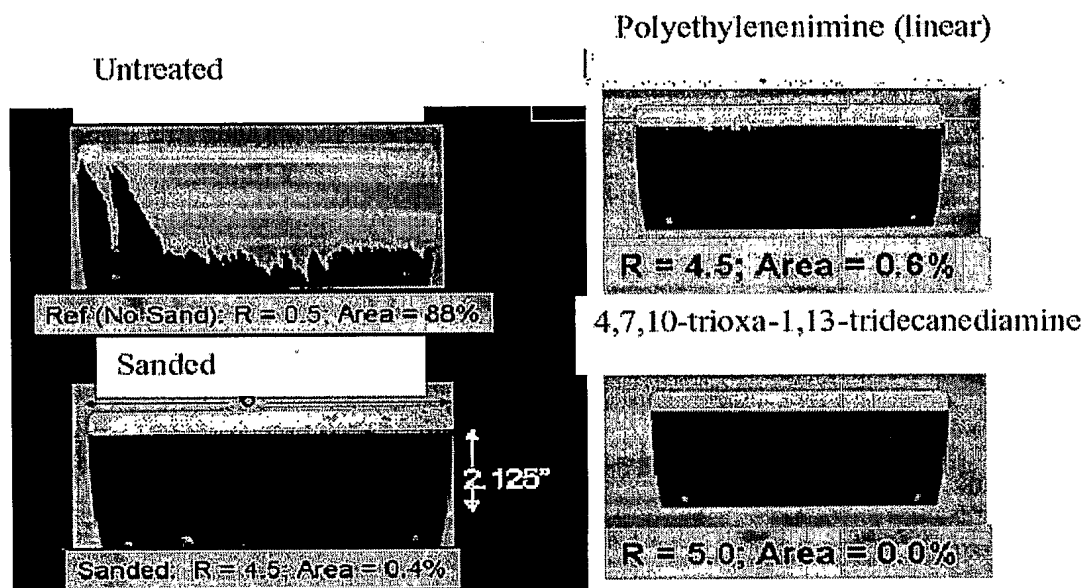


4,7,10-trioxa-1,13-tridecanediamine



polyethyleneimine
(linear)

B. Whirling arm rain erosion results of inter-coat
adhesion of aged polyurethane coatings (49°C, 18h) which
were then over-coated with blue polyurethane top-coat
5 (activation solution 50% adhesion promoter in ethyl



acetate)

Results indicate:

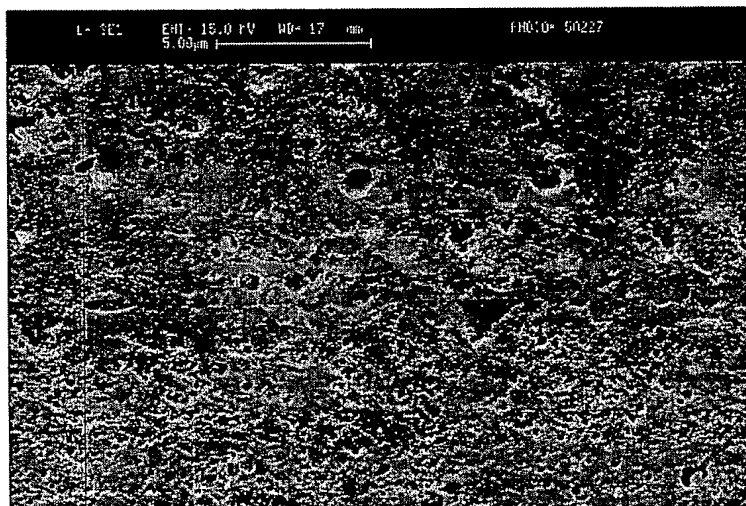
Analysis by SIJA and whirling arm rain erosion
10 experiments indicate that inter-coat adhesion of specimens
activated with suitable adhesion promoter and solvent is
comparable to the performance obtained by sanding aged
polyurethane coating prior to over-coating. In terms of
rain erosion analysis: 88% of the over coat is removed
15 from untreated samples, 0.4% from sanded, 0.6% from sample
chemically activated with PEI and 0% with those activated
with 4,7,10-trioxa-1,13-tridecanediamine prior to over-
coating. In terms of SIJA experiments assessment of the
paint area removed indicated that 177 mm² of the over coat
20 is removed from untreated samples, 13 mm² from sanded,
28 mm² from sample chemically activated with PEI and 13 mm²

with those activated with 4,7,10-trioxa-1,13-tridecanediamine prior to over-coating.

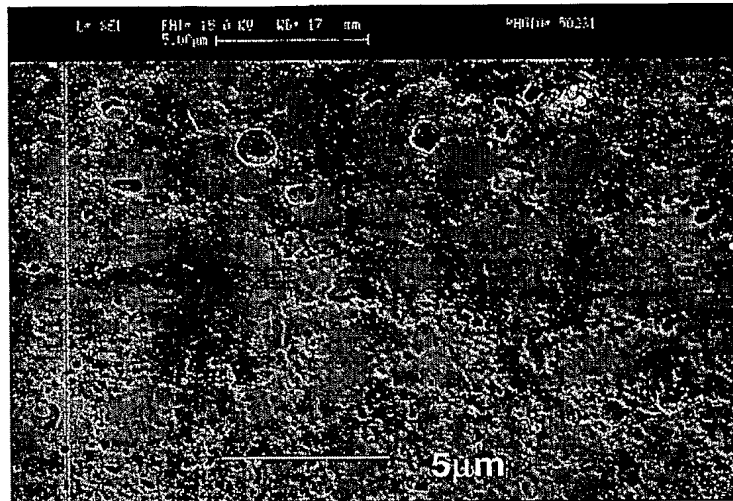
Example 15

5 SEM analysis of inter-coat adhesion of specimens painted with white polyurethane cured / aged for 18h at 49°C and activated prior to over-coating with blue polyurethane:

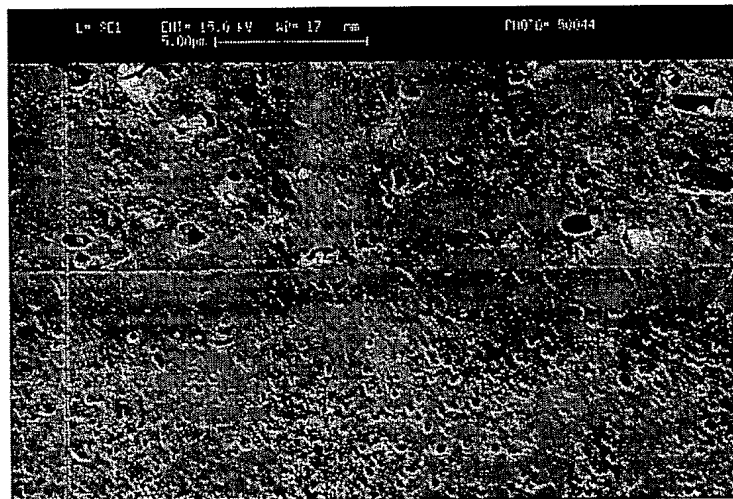
- A. 18h at 49°C prior to over-coating
- 10 B. 18h at 49°C and then sanded prior to over-coating
- C. 18h at 49°C and then treated with amine terminated polypropylene glycol (Mn 230, 50%, 60 min) in benzyl alcohol prior to over-coating



15 A.



B.



C.



5

Results indicate:

Poor inter-coat bonding in A. with voids, cracks and de-lamination between the coatings. Additional coat does not appear to wet the aged white existing coating layer.

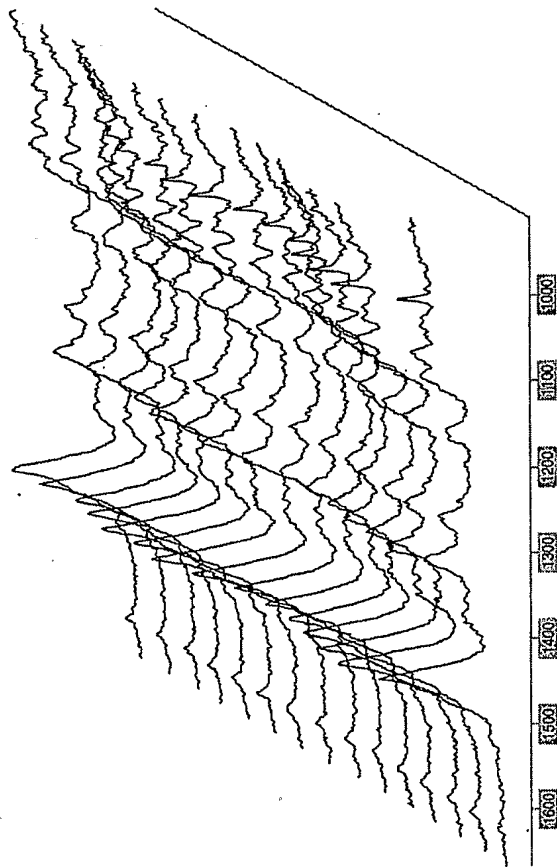
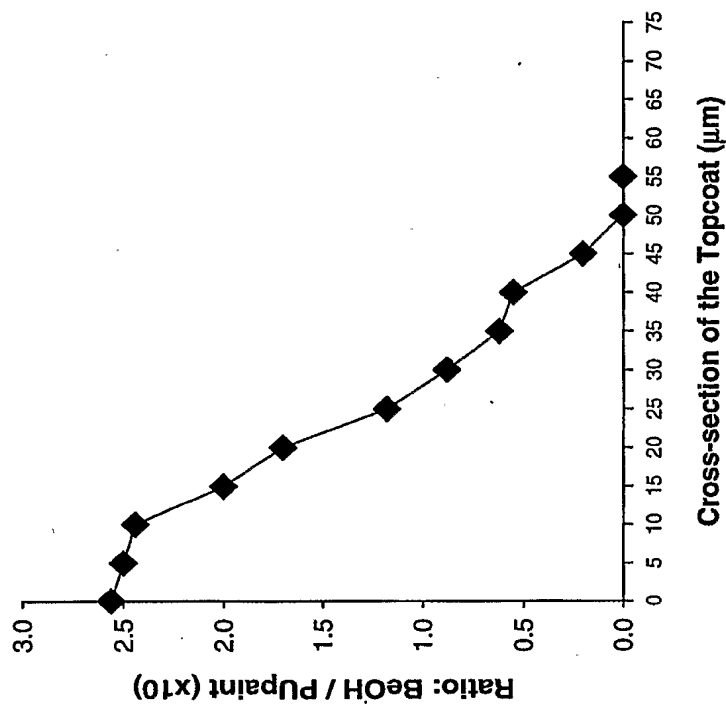
10 Good inter-coat adhesion in B. when the sample has been sanded prior to re-painting.

Good inter-coat adhesion in C. when sample has been chemically activated prior to over-coating.

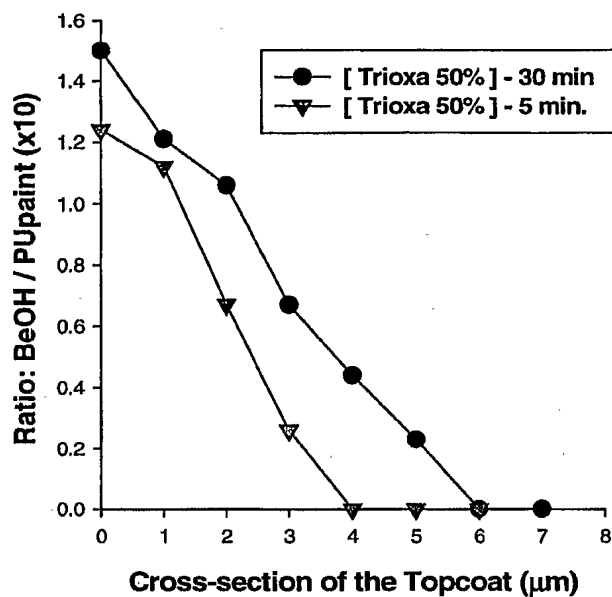
In both Examples 15 B & 15 C the fresh coating appears to wet the aged coating well.

Example 16

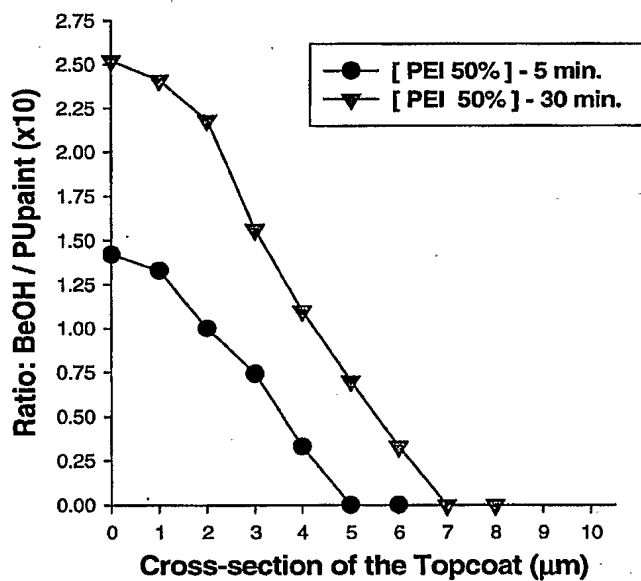
Penetration depth of various chemical activation treatments into the paint film as determined by raman spectroscopy through the ratio of benzyl alcohol ($\sim 1000\text{ cm}^{-1}$) and polyurethane CH_2 (1450 cm^{-1}) peaks



A. Benzyl alcohol only (30 min exposure)



B. 4 ,7,10-trioxa-1,13-tridecanediamine in benzyl alcohol (50%)



5 C. Polyethylene imine (linear, Mw=425) in benzyl alcohol (50%)

Results indicate:

Unlike benzyl alcohol when used on the painted surface alone, solutions of 4,7,10-trioxa-1,13-tridecanediamine or polyethylene imine in benzyl alcohol even after 30 min exposure time penetrate the paint film less than 7 micron (re: 55 micron for benzyl alcohol alone). This indicates that the activation treatment is limited to the coating surface through the appropriate choice of solvent/s adhesion promoter/s and adhesion promoter/s concentration.

Example 17

XPS analysis of a polyurethane coating before and following surface treatment in Dichlormethane.

Treatment	% Carbon	% Oxygen	% Nitrogen
Untreated (average of 3 batches)	78.2	19.8	2.0
60 min Treatment			
Amine-terminated polypropylene glycol Mn=230, 10%	70.5	26.1	3.4
Amine-terminated polypropylene glycol Mn=230, 50%	66.3	26.7	3.7
180 min Treatment			
Amine-terminated polypropylene glycol Mn=230, 10%	69.2	28.1	2.7
Amine-terminated polypropylene glycol Mn=230, 50%	68.5	28.2	3.3

XPS analysis of a polyurethane coating before and following surface treatment in benzyl alcohol.

5

Treatment	% Oxygen	% Nitrogen
Untreated	27.9	5.5
60 min treatment		
Polyethylene imine (Linear) Mw 425	25.7	8.9
Polyethylene imine (branched) Mw 800	25.5	8.5

Results indicate:

10 Changes in elemental composition occur on treatment of an aged polyurethane surface (49°C, 18h) following treatment with appropriate activation solution. The changes in elemental composition are consistent with adhesion promoter being embedded or bonded to the coating.

15

It will be appreciated by persons skilled in the art that numerous variations and/or modifications may be made to the invention as shown in the specific embodiments without departing from the spirit or scope of the invention as broadly described. The present embodiments are, therefore, to be considered in all respects as illustrative and not restrictive.

20

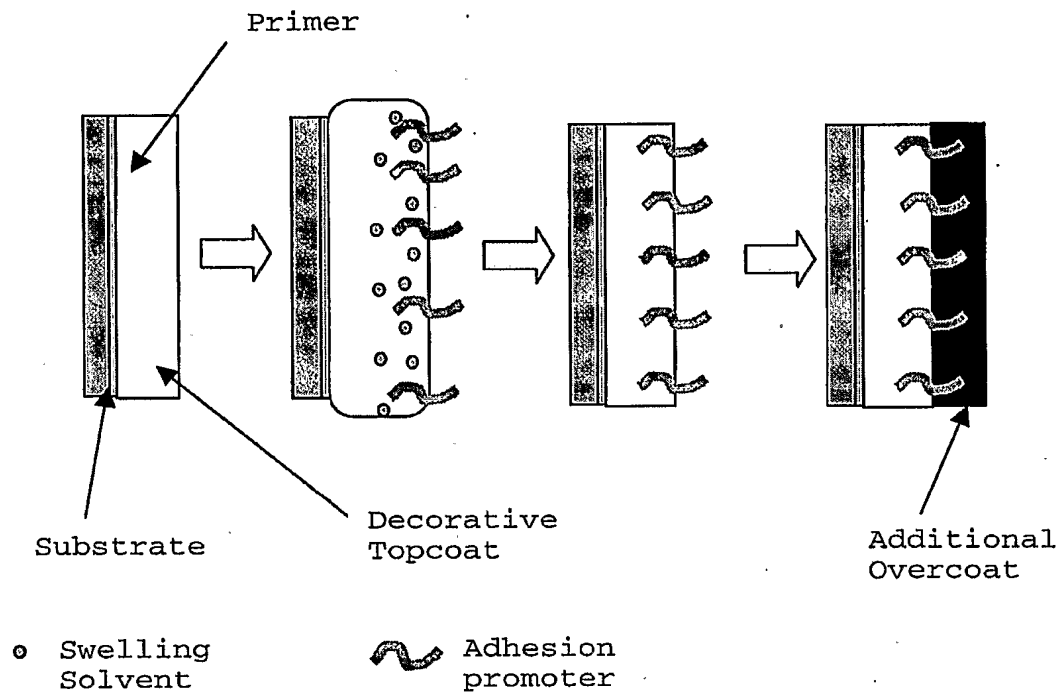


FIGURE 1: Schematic of General Activation Strategy

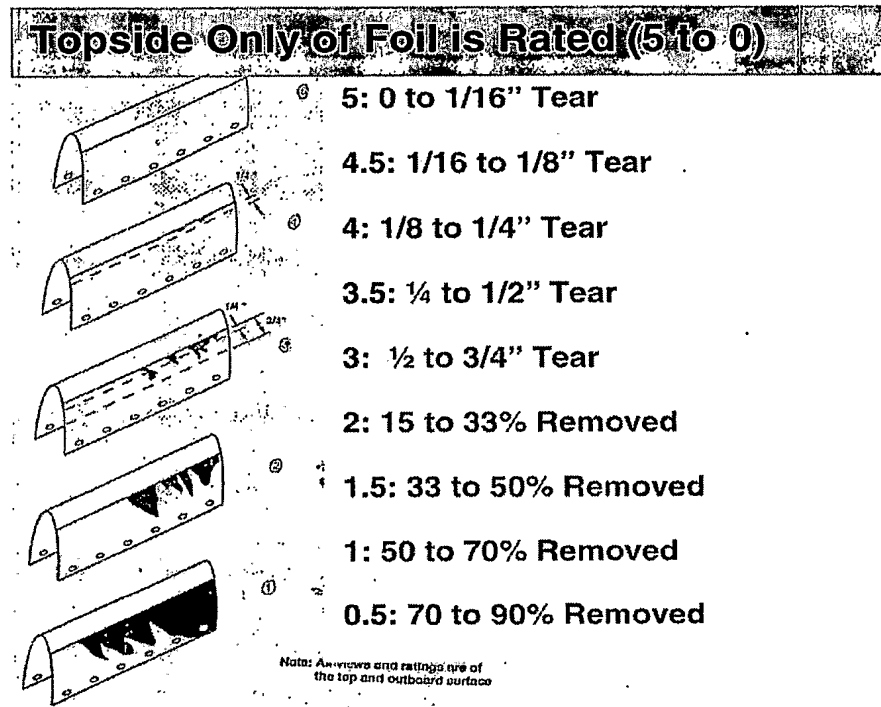


FIGURE 2: Whirling Arm Rain Erosion Performance Assessment